#### JAGANNATH GUPTA INSTITUTE OF ENGINEERING & TECHNOLOGY JAIPUR 1/II -MID TERM PAPER ANSWER SHEET

Semester: IV Branch: RE Submitted by: Wing of She forh Subject: Analog Electronics One 1. - Englain the peedback concept in detail with suitable diagram. And - Feedback Concept :-In a beedback process, a part of autput is combined with the external input Signal. fig 1.2 presents a generalized black diagram of a predbark amplifier. The cutput quantity is sampled by a suitable sampling network and fed to a predback network and then combined with an external signal through a mixer network and bed to a pasic amplifu > to=IL Sampling RL Mixen Signal Source Basic Amplinetwork pies If feedback Vf network Vf (a) Sampling Netwark :-There are two types of sampling Valtage on current. The cutput valtage is sampled by Connecting the beedback network in shunt accross the output known as veltage sampling and autput sampled by connecting feedback network in series with output Anaun as current sampling.



(5) Mixer Network :- Like sampling, there are two ways of mixing, series mixing and shemt mixing. Following figure shares there series input and shent input connection.



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O Basic Amplipies:-This can be any of the four basic amponing the have been in the privileus Dection.

() Feedback Network :--

This is a two part network, where input side is connected to the sampling network and output side is connected to the mixer network.

Que Q. Explain the general characteristics of negative beedback amplifies in detail. Ans. Characteristics of negative beedback amplifies are as ballows-O Desensitivity of transfer amplifications :> Deedback is given by the formula - $Af = \frac{A}{1+AB}$ 

At is lessthan A by a factor (1 + AF), the factor (1 + AF) is (alled ' desensitivity' and is denoted by D. If  $AF \gg 1$ , then  $1 + AF \cong AF$  and

$$Af = \frac{A}{AB} = \frac{1}{B}$$

It is clear that Af depends only on B not on Jain without beedback A.

Strequency Distortion: - We have been that Af depends on B. Hence if the beedback network is such that it does not have any force, dependent component then averall gain is not a punction of prequency. Therefore a substantial reduction in prequency is obtained.

(3) Non linear Distantion :-If a large amplitude Signal is applied to an amplipies, then it results in distortion in the centrait signal. Such distortion produces second harmonic component which is undiscrable. Let magnitude

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of second parmonic component be 52. Men let us apply negative feedback to the amplipies. There will reduction in the amplitude of Be. let it be Bef with peedback. New

$$B_{2f} = \frac{B_2}{1 + B_2 F}$$

(9) Noire:-Noire is dépined as undésirable signals picked up and amplified by the amplifies. Let N ke the amplitude of noise in an amplipies milhaut feedback It can be sharm that with beedback applied to the arps The name will be reduced to Nf, where

$$Nf = \frac{N}{1 + Aps}$$

(5) Increased Bandwichth "-

We know that amplipies gain falls app at low and high prequencies. At low prequency, the series capacitance can not be considered as short Circuited, Do the gain balls obb At higher preguency, The shut capacitance con not be considered open circuited hence gain falls ells. The bandwidth ele the amplifies will be (fe-fi). when beedback is applied, the gain of amp' is decreated.

Anigh = Amid Inigh = Amid Inight = Amid

. amplifier with suitable diagram. 10 1 1 And - Veltage - Series beedback topology :-1 1 Circuit diagram 0 0 0 0 0 0 U RE VG=Vo O 0 Step -1 -> Type of topology used is valdageseries topology. Step-2- Input and output ckt. without feedback Input = No (Short circuited) Output = Ii = 0 (open circuited) Madified diargans > 0 0 RC . 10

Stop 3 - It require that the Securce to be therein  
Saurce, but source is already a therein Securce.  
Stop 4 and 5 -> Catulate 15 -  

$$P = \frac{feedback & signal}{Gutput & Signal} = \frac{Vf}{V_0} = 1.$$
  
 $P = \frac{feedback & signal}{Gutput & Signal} = \frac{Vf}{V_0} = 1.$   
 $P = \frac{feedback & signal}{Gutput & Signal} = \frac{Vf}{V_0} = 1.$   
 $P = \frac{feedback & signal}{Gutput & Signal} = \frac{Vf}{V_0} = 1.$   
 $P = \frac{feedback & signal}{Gutput & Signal} = \frac{Vf}{V_0} = 1.$   
 $Stop - 6 Daraw h - parametes Circuit-
 $\frac{F}{P}$   
 $\frac{F}{P$$ 

Rothie

$$Avr = \frac{Av}{1 + Av} \frac{1}{1 +$$

Que 4. Explain the depination of ascillato, and also explain the Hartley Oscillatos in detail. Ans. - Defination of Oscillatos :-An Oscillatos is basically a waveform generato, which generate an output waveform which ascillates with Constant emplitude and constant desired prequency. In short, an ascillator is an amplifies, which use a positive peedback without any externed infut Signal.

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# Hartley Obuillator :-



Construction :- O R, Re and Re resistors are used for biasmy purpose.

(2) Coupling Capacitos Cc used to black dC Signal of Coix bypans (apacitos.

AFC (Radio Frequency chock) used to
prevent radio prez. Current prom reaching dc Supply
b) Prevent dc Supply from short cht the output vallage.
The dank circuit we use two inductos and q Variable capacitor.

Marking & Inductor store energy in the farm of magnetic field while capacitor store energy in the when the supply reftage is on a current is set up in tank circuit as a result the starting reltage bos Oscillation required is provided. This current produce Ac valtage averau Lifle. A transister shift a phase by 180° and the remaining 180° is provided by tank Circuif. Then the total phase Ahilot is ef D'on 360'. 1- 2TT JLeg C. The general egg of LC ascillator is hie (Z1 + Ze + Z2) + Z1Ze (hfe +1) + Z1Z3 =0  $Z_1 = j\omega L_1$ ,  $Z_2 = j\omega L_2$ ,  $Z_0 = \frac{1}{j\omega c} = -\frac{j}{\omega c}$ hie (jwLi+jwLe-j)-w<sup>2</sup>LiLe(1+hfe)+Li=0 keep in . post equal to zerohie jw (litlet 1/ wec) =0 LITLE - WEC  $\omega = \frac{1}{\sqrt{(L_1 + L_2)C}}$  $=)f=\frac{1}{2\pi \sqrt{(L_1+L_2)c_1}}$ 

Lo determine Condition of ascillation read part Should be zero.

=) - w2 Lile(1+hfe) + Li =0  $\omega^2 Le(1+hre) = \frac{1}{C}$  $\omega^{\prime 2} = \frac{1}{(1 + hfe) leC}$  $(L_{1}+L_{e})R = (h_{fe}+1) \log (1 + h_{fe})L_{e} = L_{1}+L_{e}$   $= \int h_{fe} = \frac{L_{1}}{L_{e}}$ 

One 5. Cakulate D, Gmt, A.F, Rif, Rof, R'of pos the Circuit Ahoun below. The transister parameter are hie = 1.1K, he= 50, hoc=he=0.

IJ \$ \$ 21 = 2.2K Ros=1K VG = - 1.2K NS

$$G_{1n} = \frac{-h_{R}}{R_{84} h_{R} + R_{R}}$$

$$G_{m} = \frac{-560}{1 \times 10^{3} + h_{1} \times 10^{3} + h_{2} \times 10^{3}} = 0.05$$

$$F = -Re$$

$$F = -Re$$

$$F = -Re$$

$$F = -1.2 \times 10^{3}$$

$$D = 1 + 156m = 1 + 1.2 \times 10^{3} \times 6.015 = 19.18$$

$$(i) \quad D = 1 + 156m = 1 + 1.2 \times 10^{3} \times 6.015 = 19.18$$

$$(ii) \quad G_{m}f = \frac{G_{10}}{D} = -\frac{0.015}{19.18} = 0.182 \times 10^{3}$$

$$(iii) \quad A_{vf} = G_{n,2} RL$$

$$= 0.182 \times 10^{3} \times 2.2 \times 10^{3} = 1.42$$

$$(v) \quad Ric = R_{2} D = (R_{8} + hie + R_{2}) D$$

$$= (1 \times 10^{3} + 1.1 \times 10^{3} + 1.2 \times 10^{3}) \times 19.18$$

$$= 632.94 \times R$$

V) Ro= and Rof = Ro, D= a Vi Rof = Raf 11 RL

$$Rof = Raf 11RL$$

$$Rof = R. RK IL$$

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#### JNIT JAGANNATH GUPTA INSTITUTE OF ENGINEERING & TECHNOLOGY JAIPUR I-Mid Term Examination Session 2017-2018 B.Tech II Year IV Semester Branch: EE Subject: CA-II

Dianen. EE	Bubjeet: CA-H
Time: 02:00-3:30	Subject Code: 4EE2A
Date: 06 -03-18	Max. Marks: 20

Attempt any four questions out of following five questions

Q.1 Explain series connection of two port network with suitable diagram.



482	Series-Ser	ries Connect	ion			
The parameters	eters of two n the terns of	of Z-port networ	rks connecte s consider th	d in series he figure 4	series connecti 9	on can be
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	¥'1	V <sub>la</sub>	Za	$V_{2a}$	1 V.2	
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		1 -18	the second	V 2h	1	
			1			
					-	
	Figure 4.9	Series-series	connection	of two 2	-port network	KS .
Using Z-Di	trameters, w	ve can write th	ie set of em	uations for	networks Za	
Comp - F						
Camp - F		$V_{1a} = Z_{11}$	$I_{1a} I_{1a} + Z_{12a}$	I <sub>2a</sub>		
Camp - F		$V_{1a} = Z_{11}$ $V_{2a} = Z_{2}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$	, I <sub>2a</sub> , I <sub>2a</sub>		
for networ	k Zs	$V_{1a} = Z_{11}$ $V_{2a} = Z_{2}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$	I <sub>20</sub> I <sub>20</sub>		
for networ	k Zs	$V_{1a} = Z_{11}$ $V_{2a} = Z_{21}$ $V_{1b} = Z_{1}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{12b}$	, I <sub>2a</sub> , I <sub>2a</sub> , I <sub>2b</sub>		
for networ	k Zs	$V_{1a} = Z_{11}$ $V_{2a} = Z_{21}$ $V_{1b} = Z_{1}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{12b}$ $I_{1b} I_{1b} + Z_{22b}$	12a 12a 12a 5 12b 6 12b		
for networ	k $Z_b$ erall networ	$V_{1a} = Z_{11}$ $V_{2a} = Z_{21}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{12b}$ $I_{1b} I_{1b} + Z_{22b}$ $I_{1b} I_{1b} + Z_{22b}$	12a 12a 12a 12b		
for networ	k Z <sub>b</sub> erall networ	$V_{1a} = Z_{11}$ $V_{2a} = Z_{21}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk $V_{1} = Z_{1}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{12b}$ $I_{1b} I_{1b} + Z_{22b}$ $I_{1b} I_{1b} + Z_{22b}$ $I_{1b} I_{1b} + Z_{22b}$ $I_{1b} I_{1b} + Z_{2b}$	12a 12a 12a 5 125 5 125 125		
for networ	k Z <sub>b</sub> erall networ	$V_{1a} = Z_{11}$ $V_{2a} = Z_{2}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk $V_{1} = Z_{1}$ $V_{2} = Z_{2}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1} I_{1} + Z_{12} I_{1}$ $I_{1} + Z_{22} I_{2}$	$\begin{array}{c} I_{2a} \\ I_{2a} \\ I_{2a} \\ b I_{2b} \\ b I_{2b} \\ I_{2} \\ I_{2} \end{array}$		(4.8%
for networ	$k Z_b$ erall networ	$V_{1a} = Z_{11}$ $V_{2a} = Z_{2}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk $V_{1} = Z_{1}$ $V_{2} = Z_{2}$ have	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1} I_{1} + Z_{12} I_{2}$ $I_{1} I_{1} + Z_{22} I_{2}$	$\begin{array}{c} I_{2a} \\ I_{2b} \\ b I_{2b} \\ b I_{2b} \\ l_{2} \\ l_{2} \end{array}$		(4.8
for networ	k $Z_b$ erall networ c 4.9, we h	$V_{1a} = Z_{11}$ $V_{2a} = Z_{21}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk $V_{1} = Z_{1}$ $V_{2} = Z_{2}$ have $I_{1} = I_{1}$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1} I_{1} + Z_{12} I_{2}$ $I_{1} I_{1} + Z_{22} I_{2}$ $I_{1} I_{1} + Z_{22} I_{2}$ $I_{2} = I_{1b} I_{2} = I_{2}$	$ I_{2a}  I_{2a}  I_{2a}  I_{2b}  I_{2b}  I_{2b}  I_{2b}  I_{2}  I_{2$		(4.85
for networ	k $Z_{b}$ erall networ	$V_{1a} = Z_{11}$ $V_{2a} = Z_{2}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk $V_{1} = Z_{1}$ $V_{2} = Z_{2}$ have $I_{1} = I_{1}$ $V_{1} = V$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1} I_{1} + Z_{12} I_{1}$ $I_{1} + Z_{22} I_{2}$ $I_{1} I_{1} + Z_{22} I_{2}$ $I_{2} = I_{1b} I_{2} = I_{2}$ $I_{2} + V_{1b} V_{2}$	$ I_{2a}  I_{2a}  I_{2a}  I_{2b}  I_{2b}  I_{2}  I_{2}  I_{2}  I_{2}  I_{2}  I_{2}  I_{2a}  I_{2b}  I_{2b}  I_{2b}  I_{2b}  I_{2b}  I_{2}  $	25	(4.89
for networ and for ov from figur	k $Z_5$ erall networ	$V_{1a} = Z_{11}$ $V_{2a} = Z_{22}$ $V_{1b} = Z_{1}$ $V_{2b} = Z_{2}$ rk $V_{1} = Z_{1}$ $V_{2} = Z_{2}$ iave $I_{1} = I_{1}$ $V_{1} = V$ $V_{2} = V$	$I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{12a}$ $I_{1a} I_{1a} + Z_{22a}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1b} I_{1b} + Z_{22}$ $I_{1} I_{1} + Z_{12} I_{1}$ $I_{1} + Z_{22} I_{1}$ $I_{1} + Z_{22} I_{2}$ $I_{1} + I_{1b} I_{2} = I_{1b}$ $I_{2} = I_{1b} I_{2} = I_{2} I_{2}$	$ I_{2a}  I_{2a}  I_{2a}  I_{2b}  I_{2b}  I_{2b}  I_{2}  I_{2}  I_{2}  I_{2}  I_{2a}  I_{2b}  I_{2b}  I_{2b}  I_{2b}  I_{2b}  I_{2}  I_{2} $	26	(4.8

	$= Z_{11a} I_{1a} + Z_{12a} I_{2a} + Z_{11b} I_{1b} + Z_{12b} I_{2b}$ $= Z_{11a} I_1 + Z_{12b} I_{2b} + Z_{12b} I_{2b}$	Contraction of the second
and	$= (Z_{11a} + Z_{11b})I_1 + (Z_{12a} + Z_{12b})I_2$ $= (Z_{11a} + Z_{11b})I_1 + (Z_{12a} + Z_{12b})I_2$ $V_2 = V_{2a} + V_{2b}$	(4.90)
By comparing eq	$= Z_{21a} I_{1a} + Z_{22a} I_{2a} + Z_{21b} I_{1b} + Z_{22b} I_{2b}$ = $(Z_{21a} + Z_{21b})I_1 + (Z_{22a} + Z_{22b})I_2$ (4.89), (4.90) and (4.91) we have	(4.91)
	$Z_{11} = Z_{11a} + Z_{11b}$ $Z_{a} = Z_{a} + Z_{a}$	
	$Z_{12} = Z_{12a} + Z_{12b}$ $Z_{21} = Z_{21a} + Z_{21b}$	
	$Z_{22} = Z_{22a} + Z_{22b}$ $\begin{bmatrix} Z_{11} & Z_{12} \end{bmatrix} \begin{bmatrix} Z_{11a} + Z_{11b} & Z_{12a} + Z_{12b} \end{bmatrix}$	
Hence	$\begin{bmatrix} Z_{21} & Z_{22} \end{bmatrix} = \begin{bmatrix} Z_{21a} + Z_{21b} & Z_{22a} + Z_{22b} \end{bmatrix}$	(4.92)

Therefore, the Z-parameters of individual series-series connected two 2-port networks are added.

Q.2 check whether the given polynomial are Hurwitz or not? (a)  $P(s) = s^4 + s^3 + 5s^2 + 3s + 4$ ANS;



(b)  $P(s) = s^4 + 3s^2 + 2$ 

Solution: Since P(s) contains only even polynomials, let us take its derivative  $P'(s) = 4s^3 + 6s$ . Now continued fraction expansion

$$4s^{3}+6s)\overline{s^{4}+3s^{2}+2}\left(\frac{s}{4}\right)$$

$$-\frac{s^{4}+\frac{6}{4}s^{2}}{\frac{3}{2}s^{2}+2}\frac{4s^{3}+6s}{4s^{3}+\frac{16}{3}s}$$

$$-\frac{2}{3}s)\overline{\frac{3}{2}s^{2}+2}\left(\frac{9}{2}s\right)$$

$$-\frac{3}{2}s$$

$$-\frac{3}{2}s$$

$$-\frac{3}{2}s$$

$$-\frac{3}{2}s$$

$$-\frac{2}{3}s$$

$$-\frac{3}{2}s$$

$$-\frac{2}{3}s$$

$$-\frac{2}{3}s$$

ANS: Since all quotients in the continued fraction expansion are positive, P(s) is Hurwitz.

Q.3 checks whether following function are PRF function.

 $Y(s) = \frac{s^2 + 6s + 10}{S + 10}$ 

ANS:

Since all the quotient terms of y(s) are real, therefore for real s, y(s) is real. Also the poles and zeros lie on the left half of the s-plane. Now let us see the positive realness of the given in j $\omega$ -domain.

$$Re[v(j\omega)] = Re\left[\frac{(j\omega)^{2} + 2(j\omega) + 20}{(j\omega) + 10}\right] \times \frac{-j\omega + 10}{-j\omega + 10}$$
$$= Re\left[\frac{j\omega^{3} + 2\omega^{2} - 20j\omega - 10\omega^{2} + 20j\omega + 200}{\omega^{2} + 100}\right]$$
$$= \frac{-8\omega^{2} + 200}{\omega^{2} + 100}$$

Since for all values of  $\omega$ ,  $Re[y(j\omega)] \neq 0$ , that means given function is not a positive real function

Q.4 design Cauer-1 and Cauer-2 form for given transfer function.

$$Z_{LC}(s) = \underbrace{s(s^2+4)(s^2+6)}_{(s^2+1)(s^2+5)}$$

Q.5 Write short notes on following: (a) Z-parameter

#### ANS: Z parameters

We will get the following set of two equations by considering the variables  $V_1$  &  $V_2$  as dependent and  $I_1$  &  $I_2$  as independent. The coefficients of independent variables,  $I_1$  and  $I_2$  are called as Z parameters.

V1=Z11I1+Z12I2V1=Z11I1+Z12I2

The Z parameters are

Z11=V1I1,whenI2=0Z11=V1I1,whenI2=0 Z12=V1I2,whenI1=0Z12=V1I2,whenI1=0 Z21=V2I1,whenI2=0Z21=V2I1,whenI2=0 Z22=V2I2,whenI1=0Z22=V2I2,whenI1=0 Z parameters are called as impedance parameters because these are simply the ratios of voltages and currents. Units of Z parameters are Ohm ( $\Omega$ ).

We can calculate two Z parameters,  $Z_{11}$  and  $Z_{21}$ , by doing open circuit of port2. Similarly, we can calculate the other two Z parameters,  $Z_{12}$  and  $Z_{22}$  by doing open circuit of port1. Hence, the Z parameters are also called as open-circuit impedance parameters.

(b) H-parameter

ANS: h-parameters

We will get the following set of two equations by considering the variables  $V_1$  &  $I_2$  as dependent and  $I_1$  &  $V_2$  as independent. The coefficients of independent variables,  $I_1$  and  $V_2$ , are called as h-parameters.

V1=h11I1+h12V2V1=h11I1+h12V2

I2=h21I1+h22V2I2=h21I1+h22V2

The h-parameters are

h11=V1I1,whenV2=0h11=V1I1,whenV2=0 h12=V1V2,whenI1=0h12=V1V2,whenI1=0 h21=I2I1,whenV2=0h21=I2I1,whenV2=0 h22=I2V2,whenI1=0h22=I2V2,whenI1=0

h-parameters are called as hybrid parameters. The parameters,  $h_{12}$  and  $h_{21}$ , do not have any units, since those are dimension-less. The units of parameters,  $h_{11}$  and  $h_{22}$ , are Ohm and Mho respectively.

We can calculate two parameters,  $h_{11}$  and  $h_{21}$  by doing short circuit of port2. Similarly, we can calculate the other two parameters,  $h_{12}$  and  $h_{22}$  by doing open circuit of port1.

The h-parameters or hybrid parameters are useful in transistor modelling circuits (networks).

#### (s) Pole and Zero concepts

For a given general network function As), it can be expressed as the ratio of two polynomials as written below
$= F(s) = \frac{P(s)}{Q(s)} = \frac{a_0 s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}{b_0 s^m + b_1 s^{m-1} + \dots + b_{m-1} s + b_m} = 0.15$
where the coefficients $a_0$ to $a_n$ and $b_0$ to $b_m$ are real and positive for a network containing passive elements only and no controlled sources. In this equation <i>n</i> denotes the degree of numerator polynomials and <i>m</i> denotes the degree of denominator polynomials Therefore, the numerator and the denominator polynomials can be expressed in terms of their factors. For $f(x) = 0$ , the numerator has <i>n</i> roots, say $s_1, s_2, \dots, s_n$ . Similarly for the equation $Q(s) = 0$ , the denominator has <i>m</i> roots, say $p_1, p_2, \dots, p_n$ . Hence the network function can be written as:
$F(s) = \frac{P(s)}{Q(s)} = \frac{a_0(s-z_1)(s-z_2)\dots(s-z_n)}{b_0(s-p_1)(s-p_2)\dots(s-p_m)} \qquad (2.16)$
where $a_0/b_0 = H$ is a constant which is known as scale factor and $s_1, s_2, \dots, s_n$ $P_1, P_2, \dots, P_n$ are the complex frequencies. The values of s, for which $F(s)$ has zero value are called as the zeros of $F(s)$ and the values of s, for which $F(s)$ has infinite value, ar called as the poles of $F(s)$ . A finite zero or a finite pole has a finite value. The zeros ar denoted by 0 and the poles are denoted by $>$ on s-plane. The network function a completely defined by its poles and zeros if the poles or zeros are not repeated, then the function is said to be having simple poles or simple zeros. If the poles or zeros ar number of zeros equals total number of poles. If $n>m$ , then $(n-m)$ zeros are at $s = \infty$ . This can be explained easily by taking an example, so let the network function
$F(s) = \frac{f(s+2)}{(s+1)(s+2+j3)(s+2-j3)} \qquad \dots (2.17)$

ANS;

Here, the network function has two zeros at s = 0 and s = -5. Also the network function has three finite poles at s = -2-j3, s = -2+j3 and s = -1. These zeros and poles can be shown at the s-plane as shown in figure 2.6. Hence there is included a zero at  $s=\infty$ in order to make the number of zeros equal to number of poles.



€ JAGANNATH GUPTA INSTITUTE OF ENGINEERING & TECHNOLOGY JAIPUR 1 / 11 - MID TERM PAPER ANSWER SHEET £E Semester: Branch : Are: Cupta Submitted by : Subject : EM C types of MI instruments are two Ang 1. Lacre C (a) Attraction Type MI Inst. 1 ( (b) Repulsion type NI Instru ( ( Instruments. ( (a) Attraction Type MI Pointer Air damping ( ( chamber ( Money Daon ( Balance (ontro) weight weight -coil winding The flat coil is used having a nerrow slot. It also has a MI mounted. when cuerent ( feare twrough the coil, a magnetic field is ( produced and the moving tron moves. Spring control is used the air paiction damping provided with the light AI pixton which mones In a chamber. When current plans through the coil, a mag. field is produced and nioreing ( eron mones from the weaker field to stronger Repulsion type - It is also of two typesfield. (i) Radial Vane type - In this type, there are two varies which are radial stope of (b) unos. The strips are placed within the coil. the fixed vance is attached to coil & movable is to spind

UP  $(\mathfrak{A})$ Coasial vare type - In this fixed and moving Vons are sections of co-anial glinders when C the current flows through the coil the two vones are magnetized. The repulsion tends to 5 seperate the trons the resulting torque rotates 5 the moving system. C

Ane 2. Weine buidge is used for determination of frequency in terms of values of valeious baidge elements.



At balance condition  $\left(\frac{R_1}{1+jwC_1R_1}\right)R_4 = \left(\frac{R_2-\frac{1}{2}}{wC_2}\right)R_3$  $\int \frac{Ry}{R3} = \frac{R_2}{R_1} + \frac{C_1}{C_2} + \frac{1}{C_2} \left( \frac{WC_1R_2}{WC_2R_1} - \frac{1}{WC_2R_1} \right)$ Equating real and Emaginary part  $\frac{RY}{R3} = \frac{R2}{R_1} + \frac{G}{C2}$ and NCIR2 - I = 0 WGR1 = 0





Ang 4.



L) = Unbrown self Inductorice TI = resistance connected in derives with L, C = fixed standard capacito

balance At  $\Gamma_1 = I_3$ , &  $\Gamma_2 = \Gamma_c + T_y$ At salamce for loop BCEB IR3 = ICXI two . IC = II JWCR3 - () for loop ABEDA  $\Sigma_1(R_1+\sigma_1+fwL_1) = \Sigma_2R_2 + Icr - 2$ for loop CEDC IC ( r+ Inc) = I4Ry  $IC(r+1) = (I_2 - I_C)R_Y - P$ 08 from (1), 223 I, (RITO, + JULI) = I2 R2 + I, JUC R3.8 € II (RI+ SI+ JWL, - JWC ROD) = I2R2 a & I, twicks ( ~+ truc) = (I2 - I, twicks) Ry C Or I, (JWC R38 + JWC R3R4+R3) = I2R4-0 € 0 from (4) 4(5)  $= \frac{\Gamma_1}{R_2} \left( \frac{\sigma_1 + R_1 + \frac{1}{2}\omega L_1 - \frac{1}{2}\omega CR_3 \sigma}{R_4} \right) = \frac{\Gamma_1}{R_4} \left( \frac{1}{2}\omega CR_3 \sigma}{R_4} \right)$ Equality real & imaginary part

TC = Q40×10-6 Nm ang 5 TO = NBFA = 3INM stady chall condition A-TC = Ja 3 I = 240×10-6 I= 80 ×10-6A Let resultance R 50 voltage = 80×10-6R  $VOLAP/division = \frac{BOX10^{-6}}{200} R$ R = 2.5 × 106 \_2 Ang

Anan Cleopse (Depto/EE] [GEP] [Midden Exam Solution] OD Que 1. Explain hydroo power plant with neat and clean diagram. Ans. Hydro Rower Plant "-A surge tank penstack and hydraulic turkine for generation of electric energy. The hilly areas are choosen for such plant. Diagram?~ Diggram => Dam Reserveir <- Surge Jank - value tank A E Roman The plant is stabilized at the anailability of mater is large. There may be designed as the under the earth or outside the earth.

is suge tank = ne unter having the higher level at a time with high pressure. The mates body should maintain the same pressure at a constat relacity. to premet the meter hammen's to the pensteck and turking the surge tank is used. The level of meter so pressure is also changed. So meter Durge Lank is required to the handle the mates hammes and unstable pressure. is <u>Vature tank</u> :> This is placed at the near by suge tank. for the Supply of the mets to the penstock and the turking some time the two disperent value stock are used for penstack and turkine. Penstock :-> Renstock are uned to pass the mater from surge tak and welve Fank. There are made out normally steel or concrete. The wats is paned to turkine through penstock. (ii) Pensteck => in Hydrolie turbine :-> The hydro power plat the -kinetic energy in conveted into electric energy by generator. V Porver House :-> The electricity is parced to power (in) Hydrolic turbère :>

(1225 Fig: Mueloox Fusion. Readion! - $\frac{232}{920 + n} \rightarrow \frac{139}{56B9 + }$ (06 230 920+ 12 42M0

Contratad Galat Moderofes. feel Neuton -> ----0 M Coalout delation Reflecter shield Fig: Nuclear Reactors Nuclear fission A The process of popagation of practice by multiplicitian im those of each offsman is called chain reaction pluciton pours port have controlled toped of chain redian to generate erogy. D an toal nucleon fission: O un-contall nucleon fission: - 0-OE 0-0~

and a start of the Com Com Q Eschlain two part tariff 3 these part tariffe-Sol. 2 Two port torill :-In this tariff, the total charges are hased on max," domand & energy consumed. Tout KW domand Energy (KWh)-> Energy (KWW)-> E) His schroßed os, y=DX+EZ A Separate meter is reg " to record the max" demand. This tariff is used for industrial or peany loads.

Acci to this tariffe the Conguner pays Some amount in addition to Charges for wax." doward and energy Conguned, constant c Get KVV doman Energy (Kuh

Question: Expassibilition and location of power plants. List down the factors to be considered for selection of site for their not power phut: Phywey: 1. Availability of Coal: A they mal plant of 400m. Capacity requires ready 6000 tons of Coul Eveny day. - power plant should be located reary Coal miner. 2 Ash Disposal facilities. Ash comes out in hot condition and handling is difficult - The ash can be disposed into sea or pineor 3 Water availability: water consumption is more as feed water into boiler condenses and for ash disposed. Hence plant should be docated read water sougher 4 Tieransport facility: the plant should be far away from everidential area to avoid nusiance from smoke. Hy ash and noise 5 Nature of land! land (soil) should have good baseing capacity to withstand dead load of plant

7.	Distance promo loga centare: Most of the
	time the electric prover generated in a hydro
	electric power to be economical on to eximition
	the stauts and the distances should be
	carefully considered since the cost of contaction
	of togramession lines and their maintenace
	will depend upon the elaute seleted.
, Tan	
8.	Access to site: it is always a designable
	Ractor to have a good accento the
	l'ite of the plant, this factor is very

Q. quic the compasiative of study of thermal, Hydro, Nucleaus power plant. Thermal power Nuclear power Hydro power plant plant pleent. Such the second of the second O Thermal power (1) they convert (1) hydro power plant convert lay heavy meter plant convert heat og coal elements like steam energy Energy into Electrical Wienium (235) ar (water vapou energy into electrical or into electrical theat energy energy. 210000121 Sources req? to 22 Req Source U The main Sources (2) of thermal power generate cleeticity to produce is heavy metals electricity is plant is loal in bulk like wienium, water or thoseling etc. Steam 3) In theimal power (3) In Nuclear P. P. hydro power (8) plant Coal and Nuclear Reactor plant has ach Starrage is is cesed to Condenser or required for generation Convertor Cooling fromt fans

(4) Thermal power plant producer energy 5-6 gels them supply to nearly substations

The are milet it

and all all in the

(5) Its source is

(1) Nuclear power plant (4) hydro p.p is main Source is good in to produce electricity generation but in the, the bach. the worken works very Reservier protected covers is mener because a single Inindia to produced seediction attack or Electricity body to demayed part Leny hand Put (5) Sources of Nucleary a Source of p.p. also less on Hydro p. p. is not

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less day-bejday p.p. also less on after some years ewan, so it is iss production also stop in is stop due to future non-availability of Coaf in earth Surface

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# JNIT JAGANNATH GUPTA INSTITUTE OF ENGINEERING & TECHNOLOGY JAIPUR

Semester: 
$$IZ$$
  
Branch: Electrical Machine  $_{II}$   
Subject: Electrical Machine  $_{II}$   
 $Q_5$ : (alculate the highest Speed at which  
(a) SOHZ (b) 60HZ alternator can be operated?  
 $Ane - \uparrow Ns = \frac{120 f}{P J}$   
highest Speed means lowest Number of  
Pole.  
Let the minimum number of Pole is  
 $f:2$   
 $Ns = \frac{120 f}{P}$   
(a)  $Ns = \frac{120 x50}{X} = 3000 R.P.M$   
(b)  $N_s = \frac{920 x60}{X} = 3600 R.P.M$ 

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SI. Exploin the Double field renching theory of . Single phase Induction Motor ?

Ans. The clouble revolving field theory of single phase induction motors basecally states that a stationary pulsating magnetic field can be resolved into two notating magnetic fields, each of equal magnitude but acolating in opposite directions.

equation for an alterneiting magnetic field whose axis is fixed in space is genen by-

b(x) = Bmax Sincet Cos x . . . (1)

Where, Bmax is the newsimum Value of the Sinusoidally distensibuted air-gep flux.  $Sin A Cos B = \int_{a} Sin (A-B) + \int_{a} Sin (A+B)$ b(x) = 1 Bmax Sin (wt-x) + 1 Bmax Sin (wt +x) <sup>1</sup> Brax Sin(wt-~) = equation of a ver obring field moning in positive 2' direction. <sup>1</sup> Brax Sin(wt+~) = equation of a verolving field moning in negative 2' direction.<br/>
Since,

since,

2

82. Explain the starting Method of single phase 3. M Aire - single-phase Incluction motous are userally classified accoucting to the awellowy means used to start the motor. Split phase Motor 1. capacitor Stovit Motor 2. capacitor start capacitor sun motor 3. · Permanent split capacitor motos 4 shaded pole motor cententugal sweiter 5.  $(\mathbf{i})$ JY IM RA RA. Main Wain RA 7 RM XA XM Rotor 1- Phare Y supply RA XA MM reco starting hending 3 Y IM 1-phase Supply Rotue) 0 Jag XM RA m -ue Auxillary ninding ) 6 Scanned by CamScanner

(111) J IM I-phase MRM Supply NN XM RA XA RA XA Muere Steveting neuroling (iv) of inpontin RM (Rote) = C Single Phase Supply W RA XA W MM- MMstarting winchig 93. hely synchronous motor is not self-starting ? Also, explain the why Inductor motor is inherently start ?

In synchronous motors are doubly excited machine. one is 3-phase Supply given to statoe and other is DC excitation given to motor of the motor. Induction motor is inherently start not starting A single phase incluction motor consists of a Single phase winding mounted on the stator and a cage winding on the wotors when d single phase Supply is conhected to the stator winding a pulsating magnetic field is perocluced. By pulsating field we mean that the field builds up

in the opposite direction, under these condition, the rotor does not rotate due to inertion. Single phase induction motor is inherently not self stauting and it requires some special stauting means. 94. Explain reluctance motor and stepper motor? Ano - A Reluctance motor is a type of electric motor that induces non-permanent magnetic poles on the ferromagnetic evotor, The evotor does not have any winding. Torque is generated therough the phenomenon of moments with the of magnetic reluctance. Reluctance motors can deliner nevy high power density at low cost, making them ideal for many application Stepper motor -The stepper motor has a motor momement in discrete steps. The angular molation is determi-ned by the number of pulses fed into the control corciet : Each input pulse mitiates the devine Circuit which puoduces one step of angulae movement. The device may be considered as a sugetal to analogue converter. The drive cvicint has inbuilt logic which Courses appropriate helpding to be energized and deenergized by solid state switches in nequired sequential mannes.



line of regression of x on y is  

$$x - \bar{x} = \frac{Cav(H1Y)}{r_y^2} (y - \bar{y})$$
  
=>  $(x - 0.667) = \frac{1.9997}{4.333} (9 - 1)$   
=>  $x = 0.4615Y + 0.2055$   
Coefficient of correlation  $z^2 = 0.4615 \times 0.692 = 0.3194$ 

1= 0.565 2 0.57

\_\_\_\_\_ (1)  $x = \frac{1}{20} (17 - y + 2z)$ 4.  $y = \frac{1}{20} \left( -18 - 3x + 2 \right)$   $z = \frac{1}{20} \left( 25 - 2x + 3y \right)$   $(2) \qquad (3) \qquad (3)$  $Z = \frac{1}{20} \left( 25 - 23 + 33 \right)$ Taking Instial approximation as  $\chi^{(1)} = \chi^{(1)} = \chi^{(1)} = 0$  and substituting in eq.<sup>4</sup>(1)  $\chi^{(2)} = \frac{17}{17} = 0.85$ Now, substituting x<sup>(2)</sup> 0.85 and z<sup>(1)</sup>=0 in eq.<sup>7</sup> (2)  $y^{(2)} = \frac{1}{20} \left( -18 - 3 x^{(2)} + z^{(1)} \right)$  $= \frac{1}{20} \left( -18 - 3 \times 0.85 + 0 \right)$ y(2) = -1.0275 Putting x=x<sup>(2)</sup>= 0.25 & y<sup>(2)</sup>= -1.0275 - eq' (3)  $z^{(2)} = \frac{1}{20} \left[ 25 - 2 x^{(2)} + 3 y^{(2)} \right]$ = 1 [25-2×0.85+3×(-1.0275]]  $7^{(2)} = 1.0109$ <u>Second Stenations</u>  $\frac{x^{(3)}}{x^{(3)}} = \frac{1}{20} \left[ 17 - \frac{1}{2} y^{(2)} + 2 z^{(2)} \right] = \frac{1}{20} \left[ 17 - (-1.0275) + 2 \times 1.0109 \right]$  $y^{(3)}_{20} = \frac{1}{20} \left[ -18 - 3x^{(3)} + z^{(2)} \right] = \frac{1}{20} \left[ -18 - 3x \right] \cdot 0025 + 1 \cdot 0109 \right]$  $Z^{(3)} = \frac{1}{20} \left[ 25 - 2x^{(3)} + 3y^{(3)} \right] = \frac{1}{20} \left[ 25 - 2x 1.0025 + 3(-0.998) \right]$ 2(3) = 0.9998

3.

Third Steration

$$\begin{aligned} x^{(4)} &= \frac{1}{20} \left[ 17 - y^{(3)} + 2z^{(3)} \right] = 1 \\ y^{(4)} &= \frac{1}{20} \left[ -18 - 3x^{(4)} + z^{(3)} \right] = -1 \\ z^{(4)} &= \frac{1}{20} \left[ 25 - 2x^{(4)} + 3y^{(4)} \right] = 1 \end{aligned}$$

The value in second, third iterations are almost same. Therefore the solution of given system of equations are  $\chi=1, \ \gamma=-1, \ Z=1.$ 

5. Set the line to be fitted be 
$$y = 0.16x$$
 (1)  
By principle of least squares, the normal equations are  
 $2y = mat + 62x$  (2)  
 $2y = na + 62x$  (2)  
 $x = 1 = 2 = 3 + 5$  (2)  
 $x = 1 = 2 = 3 + 5$  (2)  
 $x = 1 = 2 = 3 + 5$  (2)  
 $x^2 = 1 = 4 = 9 = 16 = 25$  (2)  
 $x^2 = 1 = 4 = 9 = 16 = 25$  (2)  
 $x^2 = 5 = 1.5$   
 $xy = 5 = 1.5$   
 $y = 15 = 2.5 = 1.5$   
 $y = 3.9 = 1.5 = 1.5$   
 $y = 3.9 + 1.5 = 1.5$